S/133/61/000/012/004/006 A054/A127

The effect of the production technology on the....

as consumable electrodes. This method proved less efficient than electroslag remelting. The ingots subjected to this process have to be roughed before forging, in the same way as the conventional ingots, while this is not necessary for ingots remelted by the electroslag process. The chemical composition of E1847 steel after vacuum remelting only changed in such a way that some silicium, niobium and manganese cinder was formed, whereas after electroslag remelting there is some sulfur and silicium cinder. The silicium content decreased in the various heats by about 0.05 - 0.15%. The niobium-carbon ratio is at least 8 in the steel produced by the various methods tested and electroslag remelting. This ratio ensures a high resistance to intergranular corrosion when checked according to the AM(AM) method [FOCT6032-58 (GOST 6032-58)]. As to nonmetallic inclusions the purest grade was obtained when smelting a fresh charge with rimming and deoxidizing with aluminum powder under white slag and by adding niobium in the form of a nickel-niobium master alloy or ferro-niobium with a low silicon content, followed by electroslag remelting. The amount of nonmetallic inclusions decreased in this way by a factor of 1.5 - 4. The technological ductility of EI847 steel increased when casting took place under the conditions described above. An additional reduction of the bath at the end of the refining period by metallic calcium increases the amount of brittle silicate

Card 3/4

S/133/61/000/012/004/006 A054/A127

The effect of the production technology on the

and globular inclusions, but, at the same time also raises the steel ductility at high temperatures (this is contrary to the general opinion that inclusions lower the steel ductility). The highest degree of ductility in hot deformation (torsion) can be obtained in steel remelted with ANF-IP slag and a test slag (torsion) can be obtained in steel remelted with ANF-IP slag and a test slag containing 30% Al₂O₃, 30% CaO and 40% CaF₂. Vacuum-remelted steel is more ductile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C tile at 1,000 - 1,100°C than steel produced by electroslag remelting, at 1,150°C than steel produced by electroslag remelting, at 1,150°C than steel produced by electroslag remelting, at 1,150°C t

ASSOCIATION: Zavod "Elektrostal'" ("Elektrostal'" Plant)

Card 4/4

s/133/61/000/006/013/017 A054/A129

AUTHORS:

Vinograd, M. I., Candidate of Technical Sciences, Goncharenko, M.S.

(Deceased), Doronin, V. M., Topilin, V. V., Chernina, B. G.,

Engineers

TITLE:

Improving the technology of 3M 347 (EI347) ball bearing steel

PERIODICAL: Stal, no. 6, 1961, 543-546

In the structure of the EI347 type steel used in 1956-57 for the production of rings of 100 mm in diameter produced from steel sections or disks made of 200-300-kg ingots the ledeburite was not sufficiently divided, moreover, the amount of non-metallic inclusions was found to be too high. In order to improve the technology of this steel grade, tests were carried out with the cooperation of Candidate of Technical Sciences A. S. Sheyn, Engineers V. N. Gorskiy, V. P. Arkhipova, Ye. V. Laguntsova, S. A. Kiseleva, V. Ya. Rybakova, Technic ns I. N. Bystrik va, Ye. P. Burdyuckina, and I. P. Solodikhin. In all tests smelting took place by blowing oxygen through the bath and by bottom casting. The ladles were made of fireclay or mullite, the weight of the ingots was 300, 500 and 750 kg, from which billets 80 x 80 - 90 x 90 mm in size were made.

Card 1/4

ELIMEL DESERVABBLES AND REPORTER OF ANY SERVED

8/133/61/000/006/013/017 A054/A129

Improving the technology of 3M347 (EI347) ...

The samples cut from strips 10-12 mm thick taken from the billets were heated in a salt bath to $1,220^{\circ} + 10^{\circ}$ C with 2 min 30 sec. holding time and annealed at $680^{\circ} - 700^{\circ}$ C for 1 hour, then cooled on air. The following six variants were tested (Table 1). Table 2 shows that the steel had the lowest percentage of non-metallic inclusions when the charge consisted of 35-60% high-speed steel scraps, 30-50% UX 15 (ShKh15) steel waste with the addition of 5-10% ferroulloys. In order to assess the effect of the ladle lining on the impurities, variant II was poured in a chamotte ladle, variant V in a mullite ladle and variant VI in a ladle lined with smooth ("planed") mullite. The best results were obtained with the mullite-lined ladle, the worst results with the ladle lined with smooth high-silicon bricks. It was established concerning the temperature that least siliceous and globular inclusions were found in the steel cast at 1,570 - 1,600 °C. The cleanest zone in the 500-kg and 750-kg ingots is that under the riser head, whereas the part containing most impurities was found in the center of the ingot. In order to obtain the required degree of non-uniformity in carbide structure of the steel, 750-kg ingots have to be used for the disks and 500-750kg ingots for sectional steel 60-80 mm in diameter, while 300-kg ingots must be taken for sections with smaller diameter. In order to remove the surface defects, the ingots had to be cleaned to a depth of 5-8 mm. By applying this new

Card 2/4

S/133/61/000/006/013/017 Improving the technology of 34347 (EI347) ... A054/A129 technology for EI347 grade steels, the waste in the finished product was less than 2%. There are 3 figures and 4 tables. ASSOCIATION: TsNIIChM and zavod / parameters "Elektrostal'" (Elektrostal' ٧I 11 Ш ١٧ Plant) Состав шихты, % Table 1: Variants of smelting and pourотходы сталей: д быстрорежу-щей . . ing EI347 grade steel: 25—30 45—50 10—20 20—25 35—60 35—40 25—30 40—45 40—45 40—45 35—50 35—45 1 - composition of the charge, Legend: 3 шхіз вольфрами-%; 2 - scraps of high-speed steel; 3 - steel, ShKhl5; 4 - Tungsten-steel* ingots, 5 - soft iron; 6 - ferro-alloys; стые шихтовые слитки 15-20 30-40 ≨ мягкое железо 15--20 15-20 10-15** 7 - lining of the ladle***; 8 - number С ферросплавы 5-10 10-15 5-10 5-10,10-15 5—10 отеровка шей*** ковof castings, (ingots) having a weight MC Ш м of, kg:; * Approximate composition: Количество пла-0.76% C; 0.25% Si; 0.28% Mn; 0.03% S; 0.03% P; 2.4% Cr; 9.55% W; 0.70% V; 0.19% Mo; ** Including 8% of 1Kh13 steel; вок, разлитых на слитки ве-COM, KE: 300 *** W = Sh: chamotte; M = M: mullite; 1 3 24 500 10 Card 3/4

小型 医动脉状态 医无法学 医性性结肠性神经神经神经病 化合物 计多点 。

S/125/61/000/001/008/016 A161/A133

AUTHORS: Vorob'yev, Yu.K., Doronin, V.M., Klyuyev, M.M., Topilin, V.V., Shiryayev, N.A., Voynovskiy, Ye.V., Medovar, B.I., Latash, Yu.V. Maksimovich, B.I.

TITLE: The effect of electro-slag remelting on the quality of chrome-nickel molybdenum 3N 847 (EI847) steel

PERIODICAL: Avtomaticheskaya svarka, no. 1, 1961, 52-56

TEXT: The authors present the results of experiments carried out with arc furnace, vacuum furnace, and electro-slag processes. The chemical composition of the EI847 grade steel is (%): 0.10-0.15 C, 14-17 Cr, 14-16 Ni, 2.5-15 Mo, 0.45-0.85 Nb, not over 0.8 Si; 0.8 Mn, 0.02 S and 0.03 P. It is austenitic, is used mainly for seamless pierced and rolled tubes, and the austenitic, is used mainly for seamless pierced and rolled tubes, and the austenitic ductility at high temperature is of primary importance. The austenitic ductility at high temperature is not subjected to $\gamma \rightarrow \alpha$ transformation at high structure of this steel is not subjected to $\gamma \rightarrow \alpha$ transformation at high cold deformation or any heat treatment. The surplus component is carbonical

Card 1/5 3

S/125/61/000/001/008/016 A161/A133

The effect of electro-slag remelting ...

Card 2/5 3

tride. Cubic Cr23C6 carbide and the intermetallic MoFe2 phase were revealed along with Nb carbonitride by X-ray analysis after long aging at 600-700°C. Aging for 500-7,000 hours at 550-700° does not cause any tendency to intercrystalline corrosion when EI847 steel is preliminarily hardened. The 100-hour strength limit for hardened EI847 steel is 25 kg/mm at 650°, and 30 kg/ $^{\circ}$ mm² at 600° . In the tests electro-slag remelting was carried out in a ρ -909 (R909) unit, in a 250 mm diameter crystallizer; the consumable electrodes were forged rods 140 mm in diameter, cleaned with emery wheel. No defects of any kind were found in ingots prepared by electro-slag remelting (Fig.2). Ingots produced by arc remelting in the vacuum were nearly as sound. The presence of globular inclusions is apparantly due to the high contamination of the initial metal before remelting. The steel produced by electro-slag and vacuum remelting had a higher ductility than steel melted by any arc furnace process (Fig.4); electro-slag remelted steel was less subject to overheating (its ductility remained at same level up to 1,300°C. Conclusions: 1) Purest (from nonmetallic inclusions) EI847 steel melted in arc furnaces was obtained in the process with a fresh charge with rimming and slag deoxidation by aluminum powder, and by employing Ni-Nb alloys, or ferroniobium with a low Si content. This process ensures the best ductility of the steel

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

The effect of electro-slag remelting ...

3/125/61/000/001/008/016

at high and ordinary temperatures. 2) If very high purity is required the E1847 steel must be melted using either the electro-slag or vacuum arc remelting with consumable electrodes. Both these methods result also in the highest technological ductility. 3) Ingots produced with the electro-slag process differ from ordinary ingots by a more dense structure, absence of pipes, loose center structure, segregation and other defects. 4) The ultimate strength of EI847 steel slightly decreases after electro-slag remelting, and the yield limit increases. The higher yield limit is due to a decreased dendritic heterogeneity owing to the particular crystallization conditions in water-cooled copper ingot molds. There are 4 figures.

ASSOCIATION: Ordena Lenina zavod "Elektrostal" im.I.F. Tevosyana (Order of Lenin "Elektrostal" Plant im.I.F. Tevosyan) - Yu.K. Vorob'yev, V.M. Doronin, M.M. Klyuyev, V.V. Topilin, N.A. Shiryayev, Ye. V. Voynovskiy; Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im. Ye.O. Patona ("Order of the Red Banner of Labor" (Electric Welding Institute im. Ye. O. Paton AS UkrSSR) -B.I. Medovar, Yu.V. Latash and B.I. Maksimovich

Card 3/53

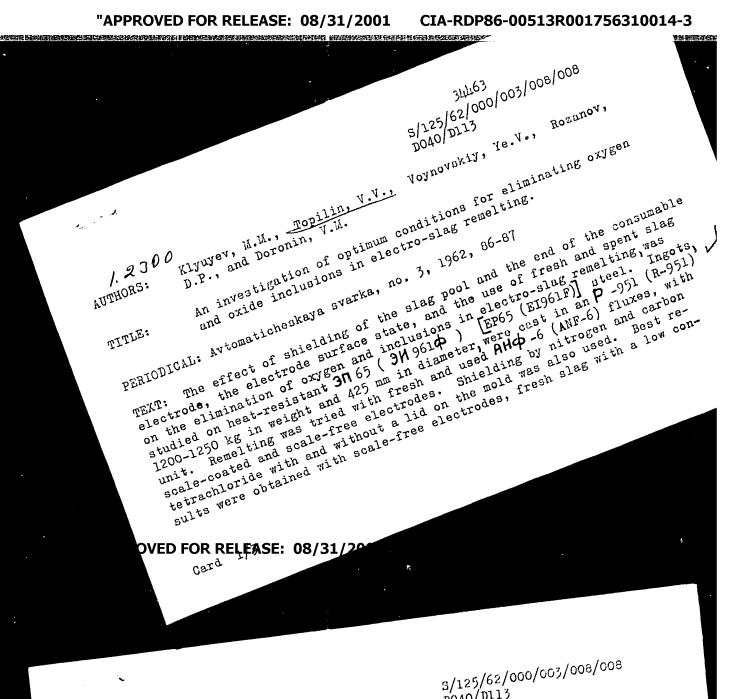
APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

KLIUEV, M.M. [Klyuyev, M.M.]; TOPILIN, V.V.

Influence of electric remelting in the slag of very richlyalloyed steels and alloys for the purpose of eliminating nonmetallic inclusions. Analele metalurgie 16 no.4:64-74 0-D

162.

"APPROVED FOR RELEASE: 08/31/2001



DO40/D113

tent of nondurable oxides (SiO2, FeO, Cr2Oz, MnO) and shielding of the slag pool. Best shielding results were obtained with a lid on the mold. The An investigation ... pool. Dest salelding results were obtained with a 11d on the mold. The oxygen content was reduced from 0.005% in the electrode to an average of oxygen content was reduced from 0.000% in the electrode to an average of 0.003% in the ingot after remelting; the content of oxide and silicate inclusions dropped by slightly over 50%. Introductions of nitrogen under the clusions dropped by slightly over 50%. Content from 0.005 to 0.005% and shielding lid further reduced the oxygen content from 0.005 to 0.005%. shielding lid further reduced the oxygen content from 0.005 to 0.002%, and the content of inclusions dropped correspondingly. It was stated that the top of electro-slag ingots, consisting of metal solidified after the furnace has been switched off, contained more oxygen than the tail portion where the oxygen content was 2-2.5 times less than in the initial metal. The use of spent slags for remelting EP65 steel does not help to eliminate oxygen and results in more globular inclusions. The composition of nonmetallic inresults in more globular inclusions. The composition of nonmetallic inclusions in comparison to the initial metal and through the height of electro-slag ingots, is different due to increased content of silica, iron oxides, chromium and manganese, and reduced alumina content. Metal remelted by electro-slag process with the use of the investigated shielding methods and impact strength in tests of longitudinal and

An investigation ...

S/125/62/000/003/008/008 D040/D113

particularly transverse specimens, as well as less anisotropic mechanical properties. It was stated that the impact strength of metal, particularly in transverse specimens, increased with diminishing content of oxide inclusions. [Abstracter's note: Complete translation].

Card 3/3

NP86-00513R001756310014-

s/148/62/600/001/005/015 E111/2435

Influence of electro-slag ...

two nickel-base heat resisting alloys of unspecified composition were also treated. Depending on the type of steel, mould diameters were 150, 250, 300, 425 mm, giving ingot weights of 100, 350, 700 and 1300 kg, respectively. Slags used were: AHΦ-6 (ANF-6) (30 to 40% Algo3, 60 to 70% CaF2); AHΦ-1Π (ANF-1P) (95% CaF₂, up to 5% CaO); CaF₂ (98% pure) and AH-29 (AN-29) (55% Al₂O₃, 45% CaO). The slag utilization coefficient (ratio of weight of metal remelted to weight of slag used) remained practically constant at 22 to 25.. In some experiments protection for the electrode tip and the slag surface was provided by a lid, with or without an inert-gas stream. original and remelted materials in the forged or rolled state were subjected to metallographic investigation; deformed metal was also used to prepare specimens for electrochemical solution and gas Oxidation was found to be an important factor in the effectiveness of inclusion elimination, e.g. with type 3065 (EP65) and 200 mm electrode diameter, the original inclusion number was 1.62, the inclusion number after remelting without any protection Card 2/5

S/148/62/000/001/005/015 E111/E435

THE SECOND SOURCE OF THE PROPERTY OF THE PROPE

Influence of electro-slag ...

with protection by only a lid over the mould and with protection by a lid and nitrogen being 1.71, 1.25 and 1.08 respectively. The first effect of protection was found to be a decrease in contamination by globular inclusions of the metal easiest to oxidize by atmospheric oxygen. Re-use of slags, if their silica and iron-oxide contents are high, leads to an increase in globular inclusions and oxygen content in the remelted metal and reduced elimination of oxide inclusions: under such conditions oxygen can be transferred to the slag/metal boundary and this explains the increase in non-metallic inclusions up to the remelted ingot. When a heat-resisting alloy with 2% Ti was remelted the silica content decreased, that of titanium nitride increased. With the $\ni \mathcal{N}$ (EI) steels the silica and iron-, chromium- and manganese-oxides contents increased, that of alumina decreased. With steels OX18H9 (OKh18N9), 3M847 (E1847) and 3M851 (E1851), when there is very little oxidation of the electrode, purification with ANF-1P is greater than with ANF-6 slag. This is due to the different conditions for flotation of the non-metallic inclusions. [Abstractor's note: Details not given.] Slag composition was Card 3/5

Influence of electro-slag ...

S/148/62/000/001/005/015 E111/E435

found also to affect the remelting rate: with OKhlôny steel the rates with ANF-IP were 85 and 100 kg/hour (0.208 and 0.244 m/hour) the corresponding figures for EI847 being 90 and 112 (0.220 and 0.270) and for LHX15CF (ShKhl5SG) (according to previous work by the authors and others) 102 and 135 (0.246 and 0.326); for this last mentioned steel rates of 182 (0.440) were obtained with Al 29 slag. Engineers V.M.Doronin, D.P.Rozanov, Ye.V.Voynovskiy, L.M.Perepelitsa as well as Laboratory assistants I.N.Eystrokova and L.M.Babkina participated in the work. There are 5 figures, 5 tables and 11 Soviet-bloc references.

ASSOCIATION: Zavod "Elektrostal'" ("Elektrostal'" Works)

SUEMITTED: September 1, 1961

Card 4/5

5/125/62/000/005/006/010 DO40/D113

Drop transfer of electrode metal in electroslag....

drops with molten slag is much greater than the contact surface area in arc steel furnaces. It appeared that electrodynamic forces (pinch effect) and surface tension have the strongest effect on drop transfer, and that these forces increase with increasing electrode diameter; this explains why the weight of drops only slightly depended on the slag bath depth. Drops were fixed on of arops only slightly depended on the slag onth depoil. It is and S was deterarmed iron electrodes, 90 mm in diameter, and the content of Si and S was deterarmed iron electrodes, 90 mm in diameter, and the content of the side of the mined in the drops, the electrode and the remelted metal. It is assumed that Si may oxidize during drop formation, and that S separates from the metal later. Conslusions: (1) Metal drop transfer from electrodes of all diameters up to 200 nm and in all studied process variations was observed. (2) The drop size increased with increasing Al O₃ content in the flux of the CaF₂-Al₂O₃ system, as well as with electromagnetic rotation of the slag and metal bath, and it did not depend on the slag bath depth. There are 5 figures and 3 tables.

Card 2/3

CIA-RDP86-00513R001756310014-3" APPROVED FOR RELEASE: 08/31/2001

S/125/62/000/005/006/010 Drop transfer of electrode metal in electroslag....

ASSOCIATION: Ordena Lenina elektrometallurgicheskiy zavod "Elektrostal" im.
I.F. Tevosyana (Electrometallurgical "Order of Lenin" "Elektrostal"

Plant im. I.F. Tevosyan)

SUBMITTED: October 24, 1961

Card 3/3

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

TOPILIN, V.V.; KLIUIEV, M.M.; VOINOVSKIY, Ye.V.; DORONIN, V.M.; ROZANOV, D.P.

Electric slag remelting of heat-resistant, stainless steels. Stal'
23 no.9:805-809 S '63.

(MIRA 16:10)

OVERSELECTED BY THE CONTROL OF THE PROPERTY OF

PANIN, V.V.; KLYUYEV, M.M.; TOPILIN, V.V.; DRUZHININA, N.P.

Investigating temperature fields in electric slag ingots. Izv. vys. ucheb. zav.; chern. met. 6 no.9:77-82 '63.(MIRA 16:11)

1. Zavod "Elektrostal".

Let $25/3 - 3 = \mathbb{E} \operatorname{Gr}(n)/\mathbb{E} \operatorname{MA}(a)/\mathbb{E} \operatorname{MP}(b)/\operatorname{The}(b) = \operatorname{LL}(a) - 1 = a_0/(1)$.

ACCESSION NR: AT4046848

\$/0000/64/000/000/0236, 9242

AUTHOR: Banny*kh, O. A., Zudin, I. F., Candidate of technical science Estalina, Ye. G., Dzugutov, M. Ya., Doronin, V. M., Topilin, V. V.

TITLE: Investigation of the phase composition and properties of chromium-manganese-

SOURCE: AN SSSR. Nauchny*y sovet po probleme zharoprochny*kh splavov. Inpledovaniya staley i splavov (Studies on steels and alloys). Moscow, Izd-vo Nauka, 1964, 236-242

TOPIC TAGS: steel structure, steel phase composition, alloy steel, steel plasticity, steel oxidation, chromium steel, manganese steel, plasticity, aluminum steel

ABSTRACT: X-ray and microstructural analyses were used to examine the structure and phase composition of 8 samples of carbon (0.5%)- manganese (15%)- aluminum (3%)- based steel with chromium (14-25%), nickel (to 3%) and copper (2.61%) additions in an attempt to develop steel brands with enhanced scale resistance. The 18-19 mm long rod-shaped samples were rolled at 1180C from 45-kg steel ingots prepared by pouring melts directly into molds at 1500-1560C. The integral intensity of the austenitic (111) line, ferritic (116) line, and (419),(212), and (411) &-phase lines were determined using an iron-emission

Card 1/2

L 13053-65

ACCESSION NR: AT4046348

URS-50I apparatus for angles of 27-30° in samples quenched from 1100C and aged at 753C for 40 hrs. The effect of hardening at 550-800C, and temperature (550-800C) and duration (to 100 hrs.) of aging on the microstructure and hardness was also investigated, and the scale-resistance was determined from weight gain by the previously described method of continuous weighing. The results show that: 1) treatment at 550-800C of steels with chromium contents in excess of 18% results in brittleness due to the formation of a 6-phase; 2) steel with less than 18% chromium retains adequate plasticity after aging at 700C; and 3) scale resistance at 900C is greater in samples with an aluminum content in excess of 2.5%, while aluminum additions at 1000C and chromium additions of 18-25% at both temperatures have little effect on scale resistance. Orig. art. has: 6 tables, 4 Harces and 1 formula.

SUBMITTED: 16Jun64

ENCL: 00

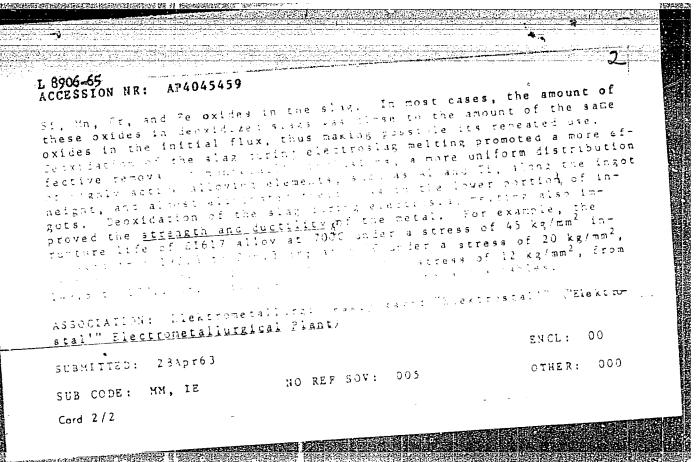
SUB CODE: MM

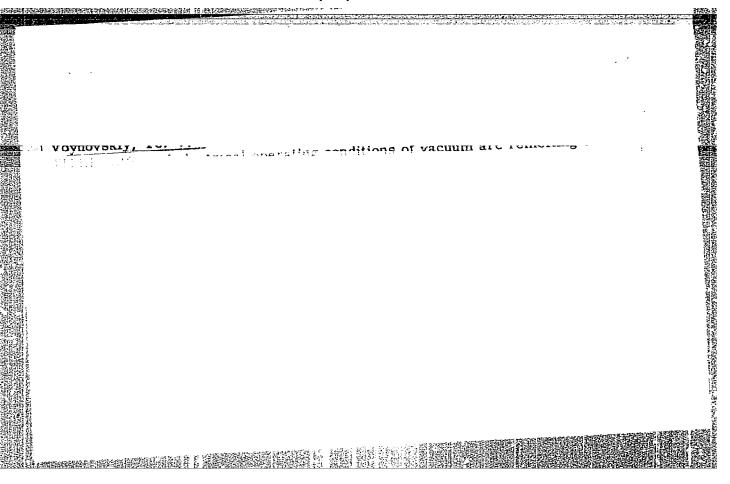
NO REF SOV: 005

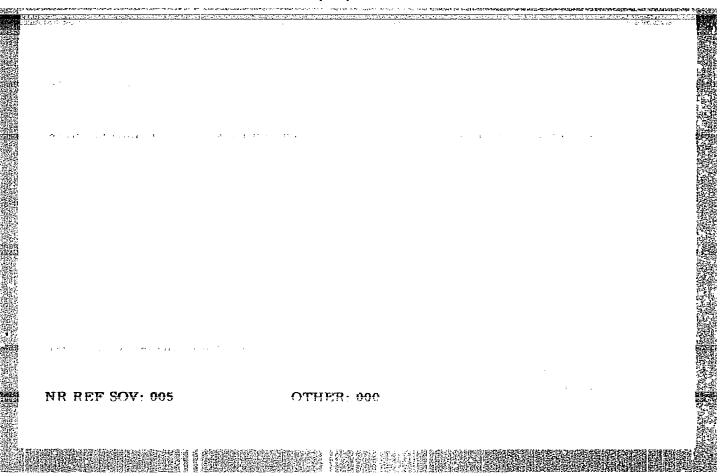
OTHER: 001

a/a

L 3906-65 FWT m T T FWT q T SWT h 1 ATT m 1 M. M. M. M. M. M. M. ACCESSION NEW APPARANCE APPARAN







\$/0279/64/000/001/0045/0047

ACCESSION NR: AP4019806

graniscoa (Pare Cr

AUTHOR: Pridantsev, H. V. (Hoscow); Stepanov, V. P. (Moscow); Topilin, V. V.

(Moscow); Klyuyev, H. H. (Moscow)

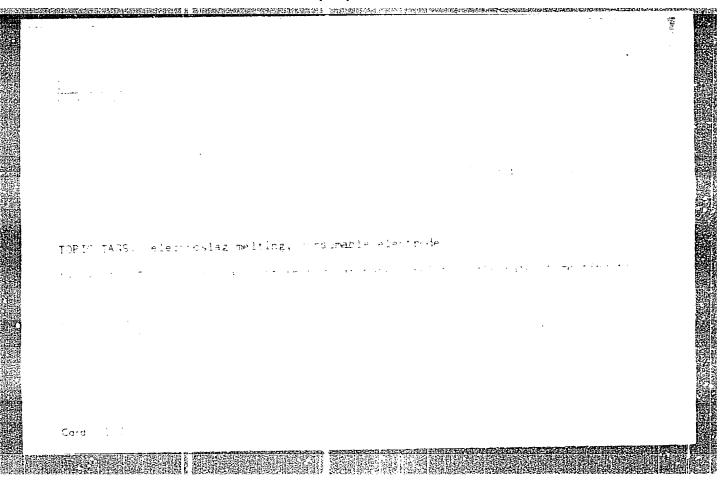
TITLE: Effect of electrosiss melting on the macrostructure of alloy KhN35VTYu

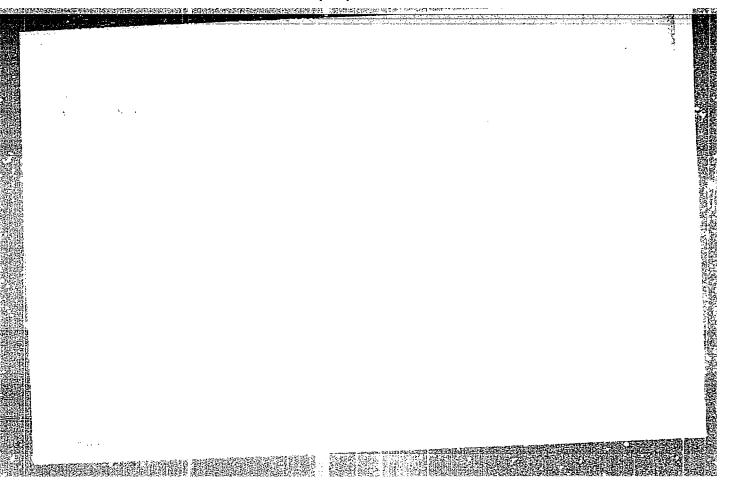
SOURCE: AN SSSR. Izv. Hetallurgiya i gornoya delo, no. 1, 1964, 45-47

TOPIC TAGS: alloy KhN35VTYu, alloy macrostructure, spotted liquation, electrosing melting, slag ANF-6, slag AN291

ABSTRACT: This economical multi-component alloy on an Fe-Cr-Ni base, designated for use under extensive stress at high temperatures and representing an excellent substitute for similar Cr-Ni based systems, is limited in its applications by a tendency to spotty liquation. The authors investigated the effects of chemical composition and the quantity of slag ANF-6 (30-40% Al₂0₃, 60-70% CaF₂) or AN₂91 (39-43% Al203, 16-20% CaF2, 22-26% CaO, 14-20% HgO), as well as of electrical current factors and electromagnetic stirring of the slag and metallic baths, on the macrostructure and surface quality of 1200-kg ingots of this alloy obtained by smelting cast or, forged electrodes (200 mm) on the P-951 apparatus in a 425-mm diameter crystallizer. It is concluded that ingots of such size can be obtained free of a potty liquation when the build-up rate is held to 165-200 kg/hr (61,v,

	ACCESSION N	IR: AP401980	6,	•		* * * * * * * * * * * * * * * * * * *	* •	
	with satisf Kernich, H.	actory macro	structure a. L. F.	. "Ye. V. Cherny*she	Voynovskiy	, N. P. D . Raskova	obtaining in ruzhinina, N. also partici	Κ.
	ASSOCIATION	l: none			· ·			
	SUBMITTED:	26Ju163		DATE ACQ:	31Mar64		ENCL: 00	
•	SUB CODE:	HL		NO REF SO	v: 004		OTHER: OOI	
		•		ا ما معمد وسفود المد	73		•	
	Card 2/2	حدود مورد			-d			



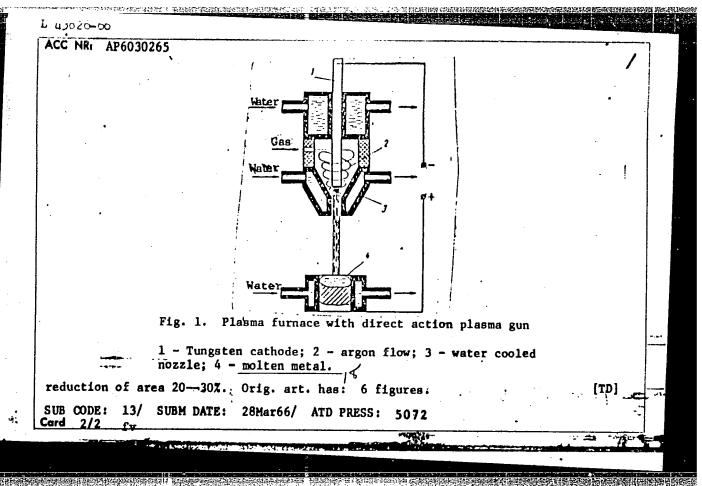


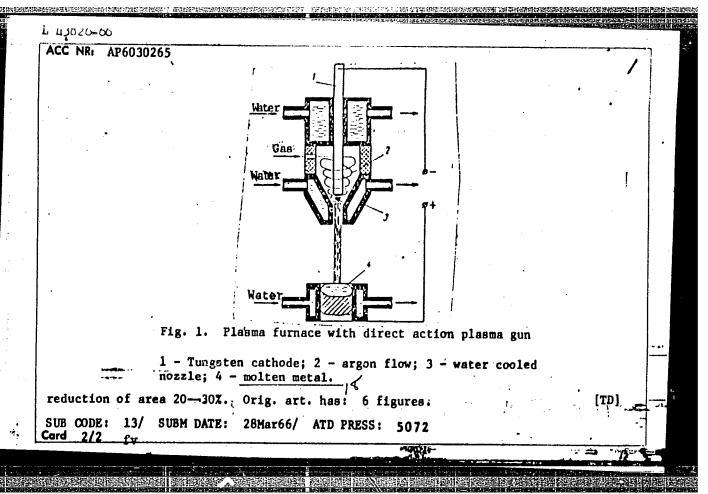
L 4177-66 EWT(a)/EWP(a)/EWP(4) (EWP(4))	
L 4177-66 EWT(a)/EWP(a)/EWP(1)/EWA(d)/EWP(v)/T/EWP(t)/EWP(k)/EWP(z)/EWP(b)/EWA ACC NR. AP5024405JD/HN/HN/HN/JGMJW(GL)/ SOURCE CODE: IP (000/1/2)	(a)
THURISTON - UR/0286/65/000/015/0083/0083	. הי
A. P. Tavetkova, V. K.; Khatalakh, R. F.; Shnyakin, N. S.; Polyakov, K. M.; Mel'nikov, Khrakovskaya, P. S. W.; Il'in, A. A.; Morozov, B. S.; Bogdanovskiy, S. P.; Topilin, V. V.; Boyarinova, Khrakovskaya, P. S. W.; Mel'nikov, ORG; none TITLE: Wrought, heat-resistant, nickel-bage and Divesting the Control of the Control o	
MINITAROVOROSES IN A TOPY WILL IN THE PROPORTY IN A WAY A TOPY AND	•
Central Scientific Research Institute of Ferrous Metallurgy im. Bardin (Tsentral'ny) Tevosyan Class 40, No. 173418 [announced by Tevosyan]	1
Al and the second secon	
SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 15, 1965, 83	
allow turned alloy, chromium containt	
17 Delyillum containing allow	i
allow with instance Certificate introduces a wronger	
alloy with improved mechanical properties and weldability. The alloy contains 17 to 0.1% max carbon, 6% max iron, 0.01% max sulfur, 0.015 max phosphorus.	
0.1% max carbon, 6% max iron, 0.01% max sulfur, 0.015 max phosphorus, 0.5% max man— SUB CODE: instantant control of the contr	
SUB CODE: MM/ SUBM DATE: OFFICE (AZ)	
SUB CODE: MM/ SUBM DATE: O5Feb64/ ORIG REF: O00/ OTH REF: O00/ ATD PRESS:4/98	
UDC: 669.245	=

和TANKATELATT / January 1982 (1984) 中国的名词复数法的现在分词 / 1984 (1984) 第一 1984 (1984)	163335
TIP(c) JT/WB/JD	
L 43942-66 EWT(d)/EWT(m)/T/EWP(f)/EWP(t)/ETI IJP(c) JT/WB/JD SOURCE CODE: UR/0133/66/000/008/0742/07-	45
1 43042-66 EWT(d)/EWT(m)/1/EHF(1)/EWT CODE: UR/0133/66/000/00076 FD	4 122
ACC NR: AP6027296	Chapter 1
ACC NRI APOUZIZZO	3
W. Topilin, V. V.; Verner, K. A.;	
AUTHOR: Doronin, V. M.; Topilin, V. V.; Verner, K. A.; Buynov, A. F. ORG: Elektrostal' Plant (Zavod Elektrostal'); Scientific Research Automobile and Control of the Institute (N-1. avtomobil'nyy i avtomotornyy institut); Gorky Automobile and Control of the Institute (N-1. avtomobil'nyy i avtomotornyy institut);	12
ORG: Elektrostal' Plant (Zavod Elektrostal'); Scientific Research Automobile and Org: Elektrostal' Plant (N-i. avtomobil'nyy i avtomotornyy institut); Gorky Automobil Automotive Institute (N-i. avtomobil'nyy zavod)	116
ORG: Elektrostal Plant (Lautomobil'nyy i avtomotornyy institutor,	
Automotive Institute (N-1. avious rayed)	
Automotive Institute (N-1. avtomotive your care) Plant (Gor'kovskiy avtomobil'nyy zavod)	
Plant (Got As	
Plant (Gor'kovskiy avtomobil myy haves TITLE: New steel for exhaust valves of internal-combustion engines	
TITLE: New Steel 201	
SOURCE: Stal', no. 8, 1966, 742-745	470
SOURCE: Stal, no. 0, 1700, 4	iing
manganese Concurred	
TOPIC TAGS: chromium nickel steel, steel, steel, austenitic steel, exhaust valve steel	
steel, austenitic steel, exhaust valve steel steel, austenitic steel, exhaust valve steel steel, austenitic steel, exhaust valve steel (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT: A new age-hardenable austenitic 5Kh20N4AG9 (EP 303) steel (0.50—0.60 ABSTRACT STEEL ST	0% C,
	e steel
ABSTRACT: A new age-hardenable austenitic States of No. 3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Mn/19-23% Cr/3.5-4.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Ni/and 0.3-0.5% Ni/and 0.3-0.5% N) has been developed. All 8.0-10.0% Ni/and 0.3-0.5% Ni/an	The
ABSTRACT: A heavily 23% Cr (3.5—4.5% Ni and 0.5 arbonitrides. 8.0—10.0% Mn (19—23% Cr) (3.5—4.5% Ni and 0.5 arbonitrides. 8.0—10.0% Mn (19—23% Cr) (3.5—4.5% Ni and 0.5 arbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 1 is fully austenitic and is strengthened by the precipitation of carbonitrides. 2 is a superposition of the precipitation of carbonitrides. 2 is a superposition of carbonitrides.	RC
is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened, and aged for 10—15 hr at 7700, has an steel, annealed at 11800, water quenched, and aged for 10—15 hr at 7700, has an steel, annealed at 11800, water quenched, and aged for 10—15 hr at 7700, has an steel, annealed at 11800, water quenched, and aged for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape in 30—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an is fully austenitic and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest and is strengthened by the precape for 10—15 hr at 7700, has an interest an interest and is strengthened by the pre	30, 30,
is fully autical at 1180C, water quenched, and respective tensile strength was	ree1
steel, annealed at 1180C, water quenched, and to steel, annealed at 1180C, water quenched, and 50 the respective tensile strength was steel, and 5 kg/mm ² . The st hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was hardness of 31—32. At 700, 800 and 900C the respective tensile strength was a second strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² . The standard strength was 20, 10, and 5 kg/mm ² .	
and 20 kg/mm ² and the interpret The weight increase in the lower than that of of	ther
hardness of 31—32. At 700, 800 and 9000 the was 20, 10, and 5 kg/mm. The standardness of 31—32. At 700, 800 and 9000 the was 20, 10, and 5 kg/mm. The standardness of 31—32. At 700, 800 and 9000 the steel and 20 kg/mm² and the 100-hr rupture strength was 20, 10, and 5 kg/mm². The standardness in 300 hr at 9000 amounted has high oxidation resistance. The weight increase in 300 hr at 9000 that the steel is lower than that of or 12.3 kg/m². The corrosion susceptibility of the steel is lower than that of or 12.3 kg/m². The weight loss in exhaust gases containing Pb0, Pb02, and 2Pb0-Pt valve steels. The weight loss in exhaust gases containing Pb0, Pb02, and 2Pb0-Pt valve steels. The weight loss in exhaust gases containing Pb0, Pb02, and 2Pb0-Pt valve steels. The weight loss in exhaust gases containing Pb0, Pb02, and 2Pb0-Pt valve steels.	oBr ₂ at —
12.3 kg/m ² . The corrosion susceptible spaces containing row, 50.80 g/m ² . hr fo	r
artica greels. The weight 1088 in 3047 g/m2 hr compared to	
oro asoc in 135-min test amounted to 300 g	
has high oxidate corrosion susceptibility of the late	
Card 1/2	
Cura 17	
Bellet Caracita	version server matter of the

SUB CODE: /9// SUBM DATE: none/ ORIG REF: 004/ OTH REF: 004/ ATD PRESS: 506/ precipitation hardening //	E169 steel. In tests of dimension stability, the EP303 valve grew by 0.16 mm in 215 hr compared to 0.7 mm for EP48 steel. Under operational conditions, the EP303 valves had 100% longer service life than EP48 valves. Orig. art. has: 9 figures and 2 tables.							
precipitation hardening	SUB CODE: 1911/	SUBM DATE: none/	ORIG REF:	004/ OTH REF: 00	4/ ATD PRESS:306			
precipitation hardening		·*						
	precipitation har	dening	-					
		• 6		•				
			`					
	•		•					

AUTHOR: Paton, B. Ye.; Lakomskiy, V. I.; Dudko, D. A.; Zabarilo, O. S.; Pryanishnikov, I. S.; Topilin, V. V.; Klyuyev, M. M. ORG: [Paton; Lakomskiy; Dudko; Zabarilo] Electric Welding Institute im. Yc. O. Paton, AN UkrSSR (Institute elektrosvarki AN UkrSSR); [Pryanishnikov; Topilin; Klyuyev] Elektrostal AN UkrSSR (Institute elektrosvarki AN UkrSSR); [Pryanishnikov; Topilin; Klyuyev] Elektrostal TITLE: Plasma arc melting of metals and alloys SOURCE: Avtomaticheskaya svarka, no. 8, 1966, 1-5. TOPIC TAGS: plasma arc, metal melting, plasma arc melting, plasma arc furnace ABSTRACT: A plasma arc furnace (see Fig. 1) for melting metals and alloys has been designed and built. The furnace is equipped with a PDM-3 plasma gun operating with a power input of 5-50 kw at a working voltage of 100 v and an operation of 20 v and an operation with a power input of 5-50 kw at a working voltage of 120 v and an operation with a power input of 5-50 kw at a working voltage of 120 v and an operation of 20 v and an operation with a power input of 5-50 kw at a working voltage of 120 v and an operation with voltage of 120 v. Ingots are 50-100 mm in diameter and up to 600 mm long. Several metals and alloys were melted in this furnace. It was found that the surface quality of the ingots was very high, there were no shrinkage holes, and the content of gaseous impurities was reduced significantly. For instance, the oxygen content in an NP-3 nickel (99.3% Ni+0) dropped from 17.7 10 % to 3-7 10 % and the density of the metal increased from 8.804 to 78.8424 g/cm The ingots were cold rolled from 75 mm to increased from 8.804 to 78.8424 g/cm The ingots were cold rolled from 75 mm to increased from 8.804 to 78.8424 g/cm The ingots were cold rolled from 75 mm to increased from 8.804 to 78.8424 g/cm The ingots were cold rolled from 75 mm to increased from 8.804 to 78.8424 g/cm The ingots were cold rolled from 75 mm to increased from 8.804 to 78.8424 g/cm The ingots were cold rolled from 75 mm to increased from 8.804 to 78.8424 g/cm The ingots we		L 43826-66 EVT(d)/EVT(m)/EVP(v)/T/EVP(t)/ETI/EVP(k)/EVP(h)/EVT(1) IJP(c) ACC NR. AP6030265 (N)JD/HM/HW SOURCE CODE: UR/0125/66/000/008/0001/0005
Plant im. I. F. Tevosyan (Zavod "Elektrostal") TITLE: Plasma arc melting of metals and alloys SOURCE: Avtomaticheskaya svarka, no. 8, 1966, 1-5. TOPIC TAGS: plasma arc, metal melting, plasma arc melting, plasma arc furnace ABSTRACT: A plasma arc furnace (see Fig. 1) for melting metals and alloys has been designed and built. The furnace is equipped with a PDM-3 plasma gun operating with a power input of 5—50 kw at a working voltage of 140—80 v and an open circuit a power input of 5—50 kw at a working voltage of 140—80 v and an open circuit voltage of 120 v. Ingots are 50—100 mm in diameter and up to 600 mm long. Several weals and alloys were melted in this furnace. It was found that the surface metals and alloys were melted in this furnace. It was found that the surface quality of the ingots was very high, there were no shrinkage holes, and the content of gaseous impurities was reduced significantly. For instance, the oxygen content in an NP-3 nickel (99.3% Ni+0) dropped from 1.77·10 % to 3-7·10 % and the density of the metal increased from 8.804 to 8.8424 g/cm³. The ingots were cold rolled from 75 mm to 0.10 mm with only one process annealing. In comparison with the original alloy, the formability improved 2—3 times, the rupture strength 40—60%, and elongation and		AUTHOR: Paton, B. Ye.; Lakomskiy, V. I.; Dudko, D. A.; Zabarilo, O. S.; Pryanishnikov, I. S.; Topilin, V. V.; Klyuyev, M. M.
SOURCE: Avtomaticheskaya svarka, no. 8, 1966, 1-5. TOPIC TAGS: plasma arc, metal melting, plasma arc melting, plasma arc furnace ABSTRACT: A plasma arc furnace (see Fig. 1) for melting metals and alloys has been designed and built. The furnace is equipped with a PDM-3 plasma gun operating with a power input of 5-50 kw at a working voltage of 140-80 v and an open circuit voltage of 120 v. Ingots are 50-100 mm in diameter and up to 600 mm long. Several metals and alloys were melted in this furnace. It was found that the surface quality of the ingots was very high, there were no shrinkage holes, and the content of gaseous impurities was reduced significantly. For instance, the oxygen content in an NP-3 nickel (99.37 Ni+6) dropped from 177.10-72 to 3-7.10-72 and the density of the metal in an NP-3 nickel (99.38.8424 g/cm ³ . The ingots were cold rolled from 75 mm to increased from 8.804 to 18.8424 g/cm ³ . The ingots were cold rolled from 75 mm to 0.10 mm with only one process annealing. In comparison with the original alloy, the formability improved 2-3 times, the rupture strength 40-60%, and elongation and	_	AN UKISSA (IIII F. Teyosyan (Zavod "Elektrostal")
ABSTRACT: A plasma arc furnace (see Fig. 1) for melting metals and alloys has been designed and built. The furnace is equipped with a PDM-3 plasma gun operating with a power input of 5—50 kw at a working voltage of 140—80 v and an open circuit voltage of 120 v. Ingots are 50—100 mm in diameter and up to 600 mm long. Several weetals and alloys were melted in this furnace. It was found that the surface metals and alloys were melted in this furnace. It was found that the surface metals and alloys was very high, there were no shrinkage holes, and the content of gaseous impurities was reduced significantly. For instance, the oxygen content of gaseous impurities was reduced significantly. For instance, the oxygen content in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—2% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—2% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—2% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—2% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—2% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10—3% to 3—7·10—3% and th		SOURCE: Automaticheskaya svarka, no. 8, 1966, 1-5.
inc. 621.791:669:187.6		ABSTRACT: A plasma arc furnace (see Fig. 1) for melting metals and alloys has been designed and built. The furnace is equipped with a PDM-3 plasma gun operating with a power input of 5—50 kw at a working voltage of 140—80 v and an open circuit voltage of 120 v. Ingots are 50—100 mm in diameter and up to 600 mm long. Several wetals and alloys were melted in this furnace. It was found that the surface metals and alloys were melted in this furnace. It was found that the surface quality of the ingots was very high, there were no shrinkage holes, and the content of gaseous impurities was reduced significantly. For instance, the oxygen content in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (99.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (199.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (199.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (199.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (199.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (199.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the density of the metal in an NP-3 nickel (199.3% Ni+6) dropped from 177·10 % to 3-7·10 % and the densi
Card 1/2		Card 1/2 UDC: 621.791:669.187.6





ACC NR. AF6027298 SOURCE CODE: UR/0133/66/000/008/0748/0751 65 AUTHOR: Svistunova, T. V.; Doronin, V. M.; Kruzkov, V. I.; Topilin, V. V.; Dzugutov, M. Ya.; Vinogradov, Yu. V.; Chermenskaya, N. F.; Kordonov, B. A. ORG: "Elektrostal" Plant (Zavod "Elektrostal"); TsNIIChM TITLE: Corrosion resistant nickel-based alloys SOURCE: Stal', no. 8, 1966, 748-751 TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel base alloy, fatigue strength ABSTRACT: The authors study and compare corrosion resistance of various types of corrosion in aggressive media. Methods are discussed for eliminating this phenomenon, iron-dontent in the alloys and the introduction of carbide-forming elements. The was with 1.4-1.7% vanadium. This eliminates intercrystalline corrosion in velded joints in the diloys and that intercrystalline corrosion could be eliminated by alloying NYOMEY alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. nickel-molybdenum alloys by reducing their carbon-silicon and iron content. The new Card 1/2 UDC: 669.14.018,8	2 1/220-27 J. T. B. (1/2) (1/2012) (1/2012) (1/2012)	
AUTHOR: Svistunova, T. V.; Doronin, V. M.; Kruzhkov, V. I.; Topilin, V. V.; Dzugutov, M. Ya.; Vinogradov, Yu. V.; Chermanskaya, N. F.; Kordonov, B. A. ORG: "Elektrostal'" Plant (Zavod "Elektrostal'"); TsNIIChM TITLE: Corrosion resistant nickel-based alloys SOURCE: Stal', no. 8, 1966, 748-751 TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel base alloy, ABSTRACT: The authors study and compare corrosion resistance of various types of corrosion in aggressive media. Methods are discussed for climinating this phenomenon. Among these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. Cord 1/2	ACC NRI AP6027298 SOUNCE COPY	;
ORG: "Elektrostal" Plant (Zavod "Elektrostal"); TsNIIChM TITLE: Corrosion resistant nickel-based alloys SOURCE: Stal', no. 8, 1966, 748-751 TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel base alloy, fatigue strength ABSTRACT: The authors study and compare corrosion resistance of various types of nickel-based alloys. The welded joints of these alloys are subject to intercrystalline Among, these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. It was also found that intercrystalline corrosion could be eliminated in chromium-nickel-molybdenum alloys by reducing their carbon-silicon and iron content. The new Cord 1/2	AUTHOR: Sylintum 5	
ORG: "Elektrostal" Plant (Zavod "Elektrostal"); TsNIIChM TITLE: Corrosion resistant nickel-based alloys SOURCE: Stal', no. 8, 1966, 748-751 TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel base alloy, fatigue strength ABSTRACT: The authors study and compare corrosion resistance of various types of nickel-based alloys. The welded joints of these alloys are subject to intercrystalline Among, these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. It was also found that intercrystalline corrosion could be eliminated in chromium-nickel-molybdenum alloys by reducing their carbon-silicon and iron content. The new Cord 1/2	M. Ya.; Vinogradov, Yu. V.; Chermenskaya, N. F.; Kordonov, B. A. Dzugutov,	, -
SOURCE: Stal', no. 8, 1966, 748-751 TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel base alloy, fatigue strength ABSTRACT: The authors study and compare corrosion resistance of various types of corrosion in aggressive media. Methods are discussed for eliminating this phenomenon. Among these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. nickel-molybdenum alloys by reducing their carbon-silicon and iron content. The new Cord 1/2	ORG: "Elektrostal'" Plant (Zavod "Elektrostal")	-
TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel base alloy, fatigue strength ABSTRACT: The authors study and compare corrosion resistance of various types of nickel-based alloys. The welded joints of these alloys are subject to intercrystalline Among these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. nickel-molybdenum alloys by reducing their carbon-silicon and iron content. The new Cord 1/2	TITLE: Corrosion resistant with Time Time Table 19 Table	
ABSTRACT: The authors study and compare corrosion resistance of various types of nickel-based alloys. The welded joints of these alloys are subject to intercrystalline Among these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. Cord 1/2 Cord 1/2	SOURCE: State alloys	: 1
ABSTRACT: The authors study and compare corrosion resistance of various types of nickel-based alloys. The welded joints of these alloys are subject to intercrystalline for these methods are heat treatment of the welded joints, reduction of carbon and iron content in the alloys and the introduction of carbide-forming elements. It was with 1.4-1.7% vanadium. This eliminates intercrystalline corrosion in welded joints in the found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. It was also found that intercrystalline corrosion could be eliminated in chromium-inckel-molybdenum alloys by reducing their carbon-silicon and iron content. The new Card 1/2		area area
ABSTRACT: The authors study and compare corrosion resistance of various types of nickel-based alloys. The welded joints of these alloys are subject to intercrystalline Among, these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EPh96. It was also found that intercrystalline corrosion could be eliminated in chromium— Cord 1/2 Cord 1/2	TOPIC TAGS: corrosion resistant alloy, intergranular corrosion, nickel bear	i
	Among these methods are heat treatment of the welded joints, reduction of carbon and found that intercrystalline corrosion could be eliminated by alloying N70M27 alloy up to 6 mm thick without requiring heat treatment. The new alloy is designated EP496. It was also found that intercrystalline corrosion could be eliminated in chromium— inckel—molybdenum alloys by reducing their carbon—silicon and iron content. The new	
UDC: 669.14.018,8		;
	UDC: 669.14.018,8	
		**

L 09250-07 ACC NR: AP6027298 alloy is designated EP567. Both of these new alloys have a fatigue limit of 5-7 kg/==2 at 1200°C which is 3-4 times higher than that of Kh18N9T steel. A new process is developed for melting and pressure working these alloys to satisfactory deformability. EP496 and EP567 alloys are melted in open induction furnaces with 500 and 1000 kg capacity. The ingots are worked on snagging machines until all defects are removed from their surfaces. Both alloys are difficult to machine, nevertheless, they can be roughed with much less difficulty than Kal8N1OT steel. Deformation temperatures for both alloys are given. Both of these alloys have excellent corrosion resistance in hydrochloric and sulfuric acids at various temperatures and concentrations. The welded seams of these alloys are not subject to intercrystalline corrosion and therefore can be recommended for welded sheet structures and tubes used in the chemical and petroleum industries. Orig. art. has: 6 figures, 2 tables. N SUB CODE: 11/ SUBM DATE: None/ ORIG REF: 003/ OTH REF: 005

ACC NR. AT6034459

(A)

SOURCE CODE: UR/0000/66/000/000/0228/0231

AUTHOR: Doronin, V. M.; Topilin, V. V.; Verner, K. A.; Buyov, A. F.

ORG: none

TITLE: New heat resistant steel for the exhaust valves of internal combustion engines

SOURCE: AN SSSR. Institut metallurgii. Svoystva i primeneniye zharoprochnykh splavov (Properties and application of heat resistent alloys). Moscow, Izd-vo Nauka, 1966, 228-231

TOPIC TAGS: heat resistant steel, valve, internal combustion engine

ABSTRACT: Existing steels with complete phase transformation, Types 4kh952, 4kh1052M (EII07), and EI992 have high critical points but at temperatures above 750° have low strength and insufficient corrosion resistance. For this reason, a new economically alloyed austenitic steel Type EP303 has been developed; it has the following chemical composition: 0.5-0.6% C; 8-10% Mn; 19-22% Cr; 3.5-4.5% Ni; 0.5-1.0% Mo; 0.3-0.5% N. The steel is melted in electric arc furnaces. The nitrogen is introduced in the form of nitrated ferrochrome with a content of from 1.5 to 7% nitrogen. The degree of absorption of nitrogen by the metal, at small concentrations, is about 70% of the amount introduced. With an increase in the amount introduced, the absorption drops to about 54%. The final nitrogen content in steel EP303 tends toward a constant value of

Card 1/2

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

T GO TO MITTING	luding the new of these alloys valve contruction	AT YOU'L.	'ina nau a'	17077 40		h	osion on all
	11/ SUBM DATE:	:					
			•				
			•				
						•	
	• :						
				•		·	.
			·	•	•		
•							
					٠		
Card 2/2 .		<u> </u>					

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

ACC NR AP7003870

(N)

SOURCE CODE: UR/0133/67/000/001/0039/0041

AUTHOR: Fomicheva, N. P.; Klyuyev, M. M.; Topilin, V. V.; Tuchkevich, N. M.; Doronin, V. M.; Dzugutov, M. Ya.; Terekhov, K. I.; Mikhin, T. A.

ORG: none

TITLE: Electroslag remelting of EI481 chromium-manganese-nickel heat resistant steel

SOURCE: Stal', no. 1, 1967, 39-41

TOPIC TAGS: Achromium manganese nickel steel, heat resistant steel, steel melting, electroslag melting, steel composition, steel mechanical property/EI481 steel

ABSTRACT:

Cast EI481 high-alloy heat-resistant steel (0.34-0.40% C, 7.5-9.5% Nn, 11.5-13.5% E, 7.0-9.0% Ni, 1.1-1.4% Mo, 0.25-0.45% Nb, 1.3-1.6% V, 0.3-0.8% Si) was electroslag remelted under four different slags and tested for chemical composition, nonmetallic inclusions and mechanical properties. The best results were obtained with the use of standard or with 10% lime No. 4 slag of the CaF_2 -CaO system. In all cases, electroslag remelting changed only slightly the steel composition. It decreased the content of manganese by 0.04-0.20 abs.% and of vanadium by 0.08 abs.%; the sulfur content decreased by 20-40%, but no substantial decrease was observed in the hydrogen and oxygen contents. The electroslag remelting also decreased

1/2

669.187.26

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3" ACC NR: AP7003870

the content of nonmetallic inclusions from 98.7 to 52.3·10⁻⁴% and resulted in more uniform distribution. No significant changes were observed in the mechanical properties of the electroslag remelted metal (all were above the technical requirements) but the anisotropy of the ductility characteristics decreased by 20—40%. In stress-rupture tests at 650C under a stress of 38 kg/mm², the steel remelted under No. 4 slag failed after 156 hr compared with 35 hr required for conventionally melted steel. Forged parts from electroslag remelted steel had a tensile strength of 112.0—104.0 kg/mm², a yield strength of 74.0—83.7 kg/mm², an elongation of 19.2—24.0%, a reduction of area of 31.2—43.9% and an impact toughness of 4.5—5.5 kg·m/cm². The corresponding figures for forgings of conventionally melted E1481 steel were 60 and 85 kg/mm², 15 and 20%, and 2.5 kg·m/cm². The electroslag remelting of E1481 steel can be recommended for increasing the service life of parts made from this steel. Orig. art. has: 2 tables.

SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 002/ ATD PRESS: 5115

Card 2/2

1,2300 also 1045.

S/125/60/000/010/002/015 A161/A133

AUTHORS: Medovar, B.I., Maksimovich, B.I., Latash, Yu.V., Topilin, V.V., Klyuyev, M.M., Shiryayev, N.A.

TITLE: The Effect of Electro-Slag remelting on the Quality of Stainless ()x18H9 (OKh18N9) and 1X14H19B3E (1Kh14N19V3B)(3M851 (E1851)) Steel

PERIODICAL: Avtomaticheskaya svarka, 1960, No. 10, pp. 11-18

TEXT: The article contains information on experiments with electro-slag remelting process. The material used were bars of OX18H9 (OKh18N9) steel KOmmin diameter, and FM 351 (EI851) steel 85 mm in diameter joined into bundles of three and melted in an ingot mold of 250 mm diameter. Five 300 kg ingots were cast. Two ingots were reforged into a 25x175x515 mm billet, and two into a 95 mm diameter bar; one was investigated as cast. The results of metallographic investigation are presented. There were no streaks, nor nonmetallic inclusion accumulations, and the absolute content of slag inclusions was considerably lower than in the initial metal, which was also confirmed by

7

Card 1/3

7

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

S/125/60/000/010/002/015 A161/A133

The Effect of Electro-Slag Remelting on the Quality of Stainless OX18H9 (OKh18N9) and 1X14H19E35 (1Kh14N19V3B) (314851 (EI851)) Steel

electro-chemical solving. The total gas content was twice lower than in the initial metal; the nitrogen and oxygen contents were reduced more than the hydrogen content. Apparently, oxygen is being eliminated in the process with floating oxide inclusions, and nitrogen and hydrogen can separate with bubbles forming on the surface of the growing metal grains. Nitrogen separates from metal easily when the metal contains no components forming stable nitrides (titanium, niobium). Nitrides having a higher melting point and larger volume do not coagulate and stick more easily in interaxial spaces. This explains the different quantity of nitrogen eliminated from the two steel grades. The following conclusions are made: 1) The electro-slag process considerably reduces the gas content and nonmetallic inclusions in both steel grades. 2) It raises the ductility of austenitic stainless steel grade and considerably reduces the anisotropy of mechanical properties. 3) The ductility of the remelted metal at hot deformation temperature is 30-40% higher than that of the initial one. There are 8 figures, 5 tables and 5 Soviet-bloc references. Card 2/3



S/125/60/000/010/002/015 A161/A133

The Effect of Electro-Slag Remelting on the Quality of Stainless 0X18H9 (OKh18N9) and 1X14H19836 (1Kh14N19V3B) (3U851 (EI851)) Steel

ASSOCIATIONS: Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im.Ye.

O.Patona AN USSR ("Order of the Red Banner of Labor" Electric
Welding Institute im.Ye.O.Paton of the UkrSSR Academy of
Sciences) (B.I. Medovar, B.I. Maksimovich and Yu.V. Latash);
Ordena Lenina elektrometallurgicheskiy zavod "Elektrostal'" im.
I.F.Tevosyana ("Order of Lenin" Electro-Metallurgical "Elektrostal'" Plant im.I.F.Tevosyan) (V.V. Topilin, M.M. Klyuyev and

SUBMITTED: May 5, 1960

γ

Card 3/3

•			
en e			
	•		3
	18.3200 1436, 1414,1573	8/125/60/000/009/003/017 4161/4130	
	AUTHORS: Latach, Yu.7., Wakeimovich, B. Topilin, Y.Y.	I., Medovar, B.I., Klyuyer, M.M.,	
	TITLE: Elimination of Bon-Metallic Incl Slag Remelting Process	usions from Metal in the Electro-	
	PERIODICAL: Avtomaticheskaya svarka, 19	60, No. 9, pp. 17-23	1/
·	TEXT: is known from previous works, tre reaelting process reduces the author com of sulfide inclusions drastically decrease on carried out by the Electric Welding Plant to investigate the effect of flux electro-slag remeiting of ball bearing a (The initial metal had been highly contained in the company of the content of	tent (Ref. 5, 6), and the quantity see (Ref. 5, 4). Experiments have Inetitute at the "Dneprospatestal" composition and properties in the teel grade HIM15CF (Shkh1530). sinated.) Three steel rode of 65 am	
	Cara-4/2		
			V
	·		
		,	
	in the residence of the second second second		

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

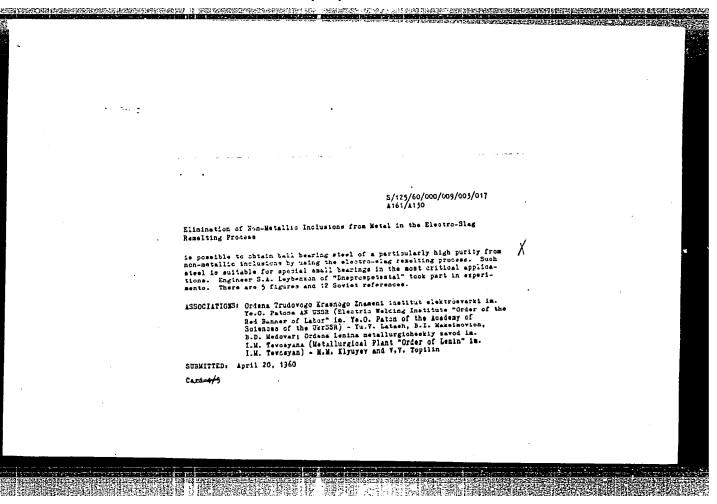
过程的主义。在1950年间125周年中共2017年间125日中共2017年1251年		
• • •	•	
	Λ.	
	•	
	5/125/60/000/009/003/017 4161/4130	
	Elimination of Non-Metallic Inclusions from Metal in the Electro-Siag Reselting Process	
	different fluxes used in the following: CaP CaO 11203	
	AHD-6 (ANF-1P)	
	Eleven ingots of 310 to 320 kg were cast. Due to the difference in conductivity of the flux grades (lowest in AN-29) the nelting rate was different (Table 2). It is exphasized that in the case of the watched ingot diameter (260 mm), the growing metting speed is accompanied by a change of grain growth direction, and the axial growth is gradually replaced by radial growth. The degree of purification from sulfides increased in the order ANY-1P, ANY-26, AN-29 flux, i.e., the highest purification was obtained with the AN-29 which had the highest CaO content. The better effect of ANY-6 than of	
• •	Car d 3/5	
	•	
3		

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

S/22/60/000/009/003/017
A15/A130

Elimination of Mon-Memballic Indicators from Metal in the Electro-Sing Researing Process

AST-IP is explained by its better desulfurising capacity due to A1.0, 1900ring the setting point of fun and rating the slad pool temperature. The
effect of AET-IP and AETA on the compant of cating a alliants and gibble
interest of AET-IP and AETA on the compant of cating a alliants and gibble
interest of AET-IP and AETA on the compant of cating a little and gibble
interest of AET-IP and AETA on the soliton, perturbatively by globules in
goin was contained anore than the bottom, perturbatively by globules in
resulting with AE-IP files. The following contained read AETA-IP and IP and I



VOROB'YEV, Yu.K.; DORONIN, V.M.; KLYUYEV, M.M.; TOPILIN, V.V.; SHIRYAYEV, N.A.; VOYNOVSKIY, Ye.V.; MEDOVAR, B.I.; LATASH, Yu.V.; MAKSIMOVICH, B.I.

是数据的保护的数据的数据。1911年,1911年的数据主题的对象主题的变形。1914年,参照对图形式。1915年中国的主题的数据的**现代的正式的现在形式的现在形式的现在分词形式的现在分词**

Effect of electric slag refining on the quality of EI847 chromiumnickel-molybdenum steel. Avtom. svar. 14 no.1:52-56 Ja '61. (MIRA 14:1)

1. Ordena Lenina zavod "Elektrostal" imeni I.F. Tevosyana (for Vorob'yev, Doronin, Klyuyev, Topilin, Shiryayev, Voynovskiy). 2. Ordena Trudovogo Krasnogo Znameni Institut elektroniki imeni Ye.O. Patona AN USSR (for Medovar, Latash and Maksimovich).

(Chromium-nickel steel—Electrometallurgy)

(Metallurgical plants—Quality control)

TOPILIN, Ye.K.

Volgograd farmers are raising agricultural standards. Zemledelie 23 no.12:7-10 D *61. (MIRA 15:1)

1. Nachal'nik Volgogradskogo oblastnogo upravleniya sel'skogo khozyaystva.

(Volgograd Province--Agriculture)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

RADOV, A.S.; SHUBIN, G.A.; TOPILIN, Ye.K.; BEGUCHEV, P.P.; GUDKOV, A.N.;
VEDENYAPIN, G.Ye.; SHUBIN, V.F.; RASKHODOV, G.F.; KAZAKWYICH, L.I.;
IVASHCHENKO, P.S.; KONUROV, S.G.; AGAPOV, P.F.; IVAHOV, A.F.

Grigorii Mikhailovich Tumin; 1876-1957. Pochvovedenie no.ll:
(MIRA 11:12)

(Tumin, Grigorii Mikhailovich, 1876-1957)

energy forested for the control of t

TOPILINA, N. P.; SAMULITSEVA, M. V. (Saratov)

Agranulocytic reaction. Klin. med. no.8:128 '61. (MIRA 15:4)

1. Iz kafedry gospital'noy khirurgii (i. o. zav. - dotsent G. N. Zakharova) lechebnogo fakul'teta Saratovskogo meditsinskogo instituta i l-y Sovetskoy bol'nitsy (glavnyy vrach P. N. Filippenko)

(AGRANULOCYTOSIS)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

USSR/Farm Attaches - Swine.

: Ref Zhur - Biol., No 13, 1953, 83445 Abs Jour

: Chirkov, D., Touiling, i. Author

Inst : Pasture Keeping of Swine in Nest Siberia. Title

Orig Pub : 3. kh. Sibiri, 1957, No 7, 51-56.

: The article deals with feethin, swine with potatoes, sugar Abstract

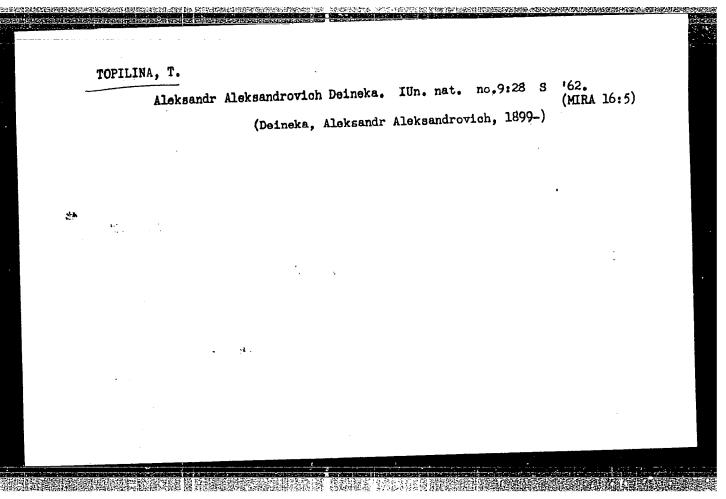
beets, lucerne grass, vetch and out mixtures, and whole

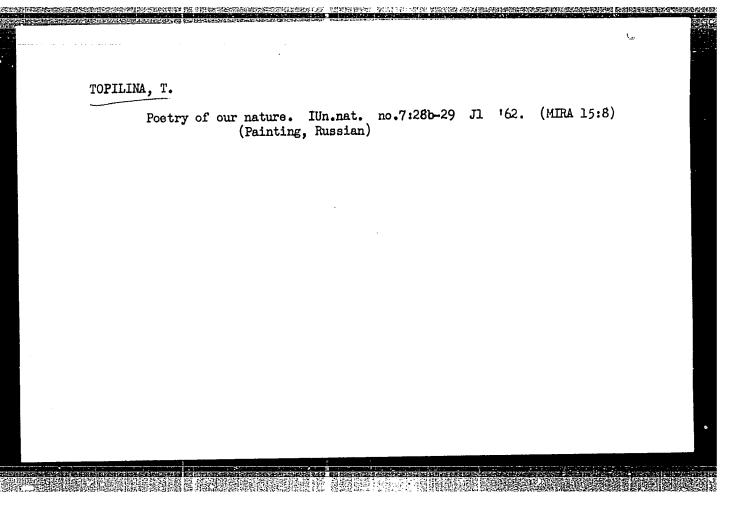
some other cultures as well.

Card 1,1

CIA-RDP86-00513R001756310014-3" APPROVED FOR RELEASE: 08/31/2001

•	





TOPILINA, Tatiyana, iskusstvoved

Light is your good ally. Sov.profsoiuzy 19 no.5:32 Hr 163.

(MIRA 16:2)

(Klectric light fixtures)

Child's initiation to the world of beauty. Sov. profsoiuzy 19 no.7:32

(MIRA 16:4)

Ap '63.

(Childred as artists)

THE REPORT OF THE PROPERTY OF

(MIRA 18:4)

AZERNIKOV, V.; ARLAZOROV, M.; ARSKIY, F.; BAKANOV, S.; BELOUSOV, I.;
BILENKIN, D.; VATEL', I.; VLADIMIROV, L.; GUSHCHEV, S.;
YELAGIN, V.; YERESHKO, F.; ZHURBINA, S.; KAZARNOVSKAYA, G.; KALININ, Yu.; KELER, V.; KONOVALOV, B.; KREYNDLIN, Yu.; LEBEDEV, L.; PODGORODNIKOV, M.; RABINOVICH, I.; REPIN, L.; SMOLYAN, G.; TITARENKO, V.; TOPILINA, T.; FEDCHENKO, V.; EYDEL'MAN, N.; EME, A.; NAUMOV, F.; YAKOVLEV, N.; MIKHAYLOV, K., nauchn. red.; LIVANOV, A., red. [Little stories about the great cosmos] Malen'kie rasskazy o bol'shom Kosmose. Izu.2., Moskva, Molodaia gvardiia, 1964.

368 p.

CIA-RDP86-00513R001756310014-3" APPROVED FOR RELEASE: 08/31/2001

TO DESCRIPTION OF THE PROPERTY OF THE PROPERTY

PISARSKI, Tadeusz; TOPILKO, Andraej

Comparative studies 2 vascular syncytial membranes of human placenta in electron and light microscopes. Ginek. Pol. 36 no. 12:1317-1325 D 1 65

1. Z I Kliniki Poloznictwa i Chorob Kobiecych AM w Poznaniu (Kierownik: prof. dr. med. W. Michalkiewicz) iz z Zakladu Aratomii Polologicznej AM w Pozaniu (Kierownik: doc. dr. med. P. Gabrost).

AB IDZHANOV, A.A.: TOPIL'SKAYA, N. V. Studying chcken coccidia in Tashkent. Uzb. biol. zhur. no.5:65-69 (MIRA 13:11)

160.

1. Institut zoologii i parazitologii AN UzSSR. (Poultry--Diseases and pests) (Tashkent--Coccidiosis)

TOPIL SKAYA Y sasluzhennyy agronom RSFSR

Over-all mechanization in the collective farm orchard. Nauka i pered.op.v sel'khoz. 9 no.9:26-29 S '59. (MIRA 13:2)

1. Direktor sovkhoza imeni 15-letiya Oktyabrya, Lipetskoy oblasti.
(Fruit culture) (Agricultural machinery)

TOPIL'SKAYA, V.S.; METLITSKIY, L.V.

Results of teamwork between a fruit state farm and a Scientific Research Institute. Kons. i ov. prom. 15 no. 12:1-3 D '60.

1. Sovkhoz imeni 15-letiya Oktyabrya Lipetskoy oblasti (for Topil'skaya). 2. TSentral'nyy nauchno-issledovatel'skiy institut konservnoy i ovoshchesushil'noy promyshlennosti (for Metlitskiy). (Canning industry)

THE STATE OF THE PROPERTY OF T

BROSS, Wiktor; KLISIECKI, Andrzej; NOWACKI, Pawel; KOCZOROWSKI, Stefan; TOPINSKI, Stanislaw; ARONSKI, Antoni

Experimental measurements of intracardiac temperature during flow of various defibriliating currents. Acta medica polona 3 no.3:231-236 162.

1. II Surgical Clinic, Medical Academy, Wroclaw Director: Prof. Dr. W. Bross Department of Physiology, Medical Academy, Wroclaw Director: Prof. Dr. A. Klisiecki The Electrotechnical Institute of the Polish Academy of Sciences, Warsaw Director: Prof. Dr. P. Nowacki. (VENTRIBULAR FIBRILLATION)

TOPIL'SKIY, K.L. (Vladivostok)

Expansion prospects for strip mining methods in the Maritime Territory. Ugol' 34 no.12:8-9 D '59. (MIRA 13:4)

(Maritime Territory-Strip mining)

Producing refined ferrochromium by the mixing of melts. Stal' 23 no.4:
331-333 Ap '63.
(Iron-chromium alloys-Metallurgy)

MOCHAR, L.I., inzhener; TOFIL'SKIY, N.A., inzhener.

Erecting electric transmission line supports by preliminary hoisting with a pipe layer. Elek.sta. 25 no.2:46 F '54.

(MIRA 7:2)

(Electric lines--Poles)

OUT HE SERVED SE

FERBEROV, Leonid Yakovlevich; TURIN, Aleksandr Aleksandrovich;

TOPIL'SKIY, Nikolay Leonidovich; GRAMMATIKOV, A.N., otv.red.;

MIROSHNICHENKO, V.D., red.izd-va; PROZOROVSKAYA, V.L., tekhn.red.

[Compiling estimates and making calculations for capital construction in the coal industry] Sostavlenie smetnoi dokumentatsii i proizvodstvo raschetov v kapital'nom stroitel'stve ugol'noi promyshlennosti. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po gornomu delu. Pt.l. [Estimates for coal-mining work] Smetnaia dokumentatsiia na gornoprokhodcheskie raboty. 1960. 261 p. (MIRA 14:6)

(Coal mines and mining-Finance)

TOPIL'SKIY, N.L., inzh.

Fossibilities for lowering the cost of rock removal in vertical shafts. Shakht. stroi. 4 no.3:5-6 Mr 160. (MIRA 13:11)

1. TSentral'nyy nauchno-issledovatel'skiy institut Podzemshakhtostroy. (Pneumatic machinery) (Mine hoisting)

TOPIL'SKIT, N.L., inzh.

Economic aspects of the mechanized loading of rocks in working horizontal tunnels. Shakht. stroi. 4 no.12:3-5 D 160. (MIRA 13:12)

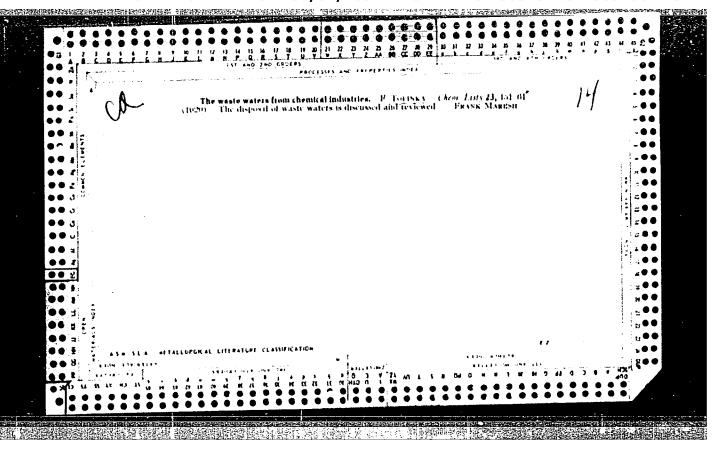
1. TSentral'nyy nauchno-issledovatel'skiy institut Podzemshakhtostroy.

(Mining engineering) (Loading and unloading)

FERBEROV, Leorid Yakovlevich; TOPIL'SKIY, Nikolay Leonidovich; IYUL'KO, Ye.V., retsenzent; GRAMMATIKOV, A.N., otv.red.

[Preparing estimates and the payment procedure for capital construction in the coal industry. Estimates for construction work, and the acquisition and assembly of equipment] Sostavlenie smetnoi dokumentatsii i proizvodstvo raschetov v kapital'nom stroitel'stve ugol'noi promyshlennosti. Moskva, Nedra. Pt.2. 1964. 341 p. (MIRA 18:2)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"



建设建筑中央企业中的设计和设备。2015年2月,1882年2月,2015年2月,1987年2月,1987年2月,1987年2月,1987年2月,1987年2月,1987年2月,1987年2月,1987年2月,1987年2

1/1

CZECHOSLOVAKIA

SOVA, J.; KARLICEK, V.; TOPINKA, I.; LANG, N.; Clinic of Internal Diseases, Medical Faculty, Charles University (Klinika Chorob Vnitrnich Lek. Fak. KU), Plzen, Chief (Prednosta) Prof Dr J. SOVA

"Influence of Histamine on Vanilmandelic Acid Excretion in Diastolic Hypertension."

Prague, Casopis Lekaru Ceskych, Vol 106, No 9, 3 Mar 67, pp 250 - 252

Abstract /Authors' English summary modified 7: Vanilmandelic acid excretion after intravenous stimulation with histamine was investigated in 7 normotonic and 10 hypertonic subjects. In normotonic subjects the excretion rose significantly, in hypertonic there was no change; even when nicotine and psychic stress were applied, no change was observed. The explanation is probably due to a disorder in catecholamine degradation and a deficiency in monoamino-oxidase activity. 2 Figures, 1 Table, 13 Western, 2 Czech references.

1/1

TOPIRCEANU, L., ing.

Impressions from the German Democratic Republic. Mec electrif agric 9 no. 4:68-70 '64.

1. Director General, Section of Repair Works.

Role and tusks of capair stations in insuring a good operating quality of the agricultural equipment. Mee electric agric 9 no.5:3-7 '64.

1. Director General, Trust of Repair Stations.

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

VOINOV, S.G.; EALTHNIKOV, Ye.S.; TOPILISKIY, P.V.; BOBKOVA, O.S.;

MINELDY V.G.: EART G. V.P.; ROSGY, L.P.; SHALIMOV, A.G.;

Prinimali uchastiys: IGFF; Y.N.; CHARGEREG, N.I.;

TARGERIE.

Developing a procedure for the making of limestone and alumina semifinished products for the preparation of synthetic slag.

Stall 22 no.2:128-132 F '62. (Slag)

(Electric furnaces)

H CZECHOSLOVAKIA/Chemical Technology. Chemical Products and Their Applications. Cellulose and Its Derivatives. Paper. Abs Jour: Ref Zhur-Khimiya, No 6, 1959, 21788 : Topinka, Vladimir : Dependence Between the Content of Water Author Inst in Wood and Its Properties. Title Orig Pub: Papir a colulosa, 1958, 13, No 7, 155-158 Abstract: The problem of the spread (accumulation) of water in wood (W) and of the interrelation between the moisture of W and its stability in displacement is examined. : 1/2 Card H-144

Η

CZECHOSLOVAKIA/Chemical Technology. Chemical Products and Their Applications. Cellulose and Its Derivatives. Paper.

Abs Jour: Ref Zhur-Khimiya, No 6, 1959, 21788

These relations have a practical value during defibering of W in the wood pulp production process. Special attention is allotted to the outlay of electrical power in defibering. -- From the author's summary.

Card : 2/2

TOPINKA, Zdenek, promovany geolog

Problems of noncore drilling in prospecting for coal deposits. Geol pruzkum 6 no.5:135-136 My '64.

1. Central Geologic Institute, Prague.

TOPINSKI, Stanislaw

Thermistor starters in D.C. motor circuits. Rozpr elektrotech 9 no.4:523-556 63.

l. Instytut Podstawowych Problemow Techniki, Polska Akademia Nauk, Warszawa.

TOPKASOV, L.P.; NEFEDOV, M.V.

Rapid assembly of shops for the production of caprolactam.
Prom. stroi. 41 no.2:10-12 F '63. (MIRA 16:3)

1. Trest Sibmetallurgmontazh.
(Kemerovo—Azepinone)
(Kemerovo—Chemical plants)

VOSKRESENSKAYA, N.T.; TIMOFEYEVA, N.V.; TOPKHANA, M.

Thallium in some minerals and rocks of sedimentary genesis.

Geokhimiia no.8:737-741 '62. (MIRA 15:9)

l. Kafedra geokhimii Moskovskogo gosudarstvennogo universiteta imeni Lomonosova.

(Thallium)

KISELEV, G., mayor; TOPILISKIY, V., mayor; GLUSHKIN, I., starshina;
UFIMMSEV, I., kapitan; PROKOP'YEV, G., starshiy leytonant;
DEREVYANKO, N., leytenant

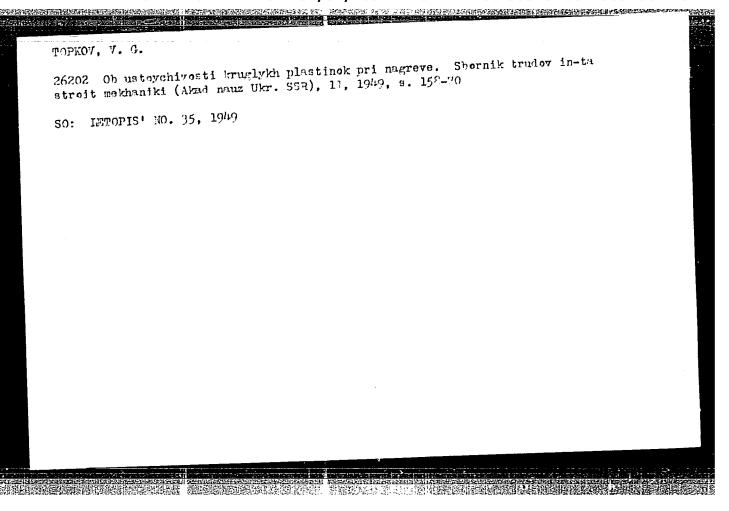
How do you train radiotelegraph operators?; discussion of the article published in No.1. Voen. vest. no.3:
0f the article published in No.1. (MIRA 17:5)
101-103 Mr'164.

TOPKOV, V. G.

26201 Sepryazheniya vo vrushchuyushchikhsya diskukh pri vysokikh temperaturakh.
Sbernik trudov in-ta streit makhaniki (Akad menz Ukr. SSR), 11, 1949, s. 144-57

SO: LETOPIS' 10. 35, 1949

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"



STOJKOV, Nevena; MILETIC-SAIN, Dimitrije; TOFLA, Dusanka

Fasciolasis hepatica. Srpski arh. celok. lek. 84 no.11:
1255-1265 Nov 56.

1. Decja klinika Medicinskog fakulteta u Beogradu. Upravnik:
prof. Milivoje Sarvan.
(DISTOMIASIS, in infant and child.
(Ser))

TOPLENINOVA, K.A.; REMEZOV, P.I.

Improving the diagnosis of rabies. Veterinaria 37 no.11:85-28
(MIRA 16:2)
(Rabies)

REMEZOV, P.I.; TOPLENINOVA, K.A.

Indirect method of fluorescent antibodies for diagnosing lymphocytic choriomeningitis. Veterinariia 38 no.9:84-86 S '61. (MIRA 16:8)

l. Voyenno-meditsinskaya ordena Lenina akademiya imeni Kirova.

TOPLEMNOVA K.N.; IVANOV, N.P.; SHMSHALING, S.V. DANSKER, V.N.; TOPLEMINOVA, K.A.

Shaterlals on the study of leptospiral jaundice. Beoort No.13: First results of specific serum therapy in Weil's disease in Leningral.

Trudy Len.inst.epid. i mikrobiol. 9:128-137 '47. (MLHA 10:9)

1. Iz leberatorii po isuchaniyu leptospirozov (zav. K.N.Tokarevich)

Lastituta epidemiologii i mikrobiologii in. Pastera (dir. F.I.Krasnik)

i Instituta vaktsin i syvoratok (dir. A.A.Sinttskiy) i infektsionnogo i Instituta vaktsin i syvoratok (dir. A.A.Sinttskiy) i infektsionnogo otdeleniya bel'nitey V.Slutskov (glavnyy vrach E.M.Abkin)

(LENINGRAD--WEIL'S DISMASE) (SERUM THERAPY)

TOPLENINOVA, K. A., REMEZOV, P. I.

Perfecting the diagnosis of rables, Veterinariya, Vol. 37, No. 11, p. 85, 1960.

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

TOPIENINOVA, K. A. and REMEZOV, P. I. (Military-Medical Academy of Order of Lenin Imeni S. M. Kirova)

The indirect method of application of flourescent antibodies for the diagnosis of lymphocytic choriomeningitis.

Veterinariya vol. 38, no. 9, September 1961, pp. 84.

TOPLENINOVA, K.A.

Use of an indirect fluorescent antibody method in the detection of the rabies virus. Vop.virus. 6 no.2:174-177 Mr-Ap '61. (MIRA 14:6)

1. Kafedra mikrobiologii Voyenno-meditsinskoy ordena Lenina akademii imeni S.M.Kirova, Leningrad.

(RABIES) (ANTIGENS AND ANTIBODIES)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001756310014-3"

REMEZOV, P.I.; TOPLENINOVA, K.A.

Detection of the lymphocytic choriomeningitis virus using an indirect fluorescing antibody method. Vop.psikh.i nevr. no.7:113-indirect fluorescing antibody method. Vop.psikh.i nevr. no.7:113-indirect fluorescing antibody method. (MIRA 15:8)

120 '61.

(MENINGITIS VIRUSES) (ANTIGENS AND ANTIBODIES)

(FLUORESCENCE MICROSCOPY)

CIA-RDP86-00513R001756310014-3 "APPROVED FOR RELEASE: 08/31/2001

ACC NR: AP6027250

SOURCE CODE: UR/0177/66/000/007/0044/0049

Bashmakov, G. A. (Major; Medical corps); Topleninova, K. A. AUTHOR:

ORG: none

·TITLE: Using fluorescent antibodies to detect tick-borne and Japanese encephalitis virus

SOURCE: Voyenno-meditsinskiy zhurnal, no. 7, 1966, 44-49

TOPIC TAGS: fluorescent antibody technique, disease diagnosis, diagnostic method, Japanese encephalitis, tick borne encephalitis, virus, virus disease, antibody, encephalitis, fluorescence

ABSTRACT:

The fluorescent-antibody technique was applied to various types of cells infected with tick-borne encephalitis virus to determine its value as a diagnostic method. This method reveals viruses in 18-48 hr depending on the types of cells atudied. Virus was detected in the medium after 24 hr, making this the fastest available method. [WA-50; CBE No. 11]

SUB CODE: 06/ SUBM DATE: none

Card 1/1

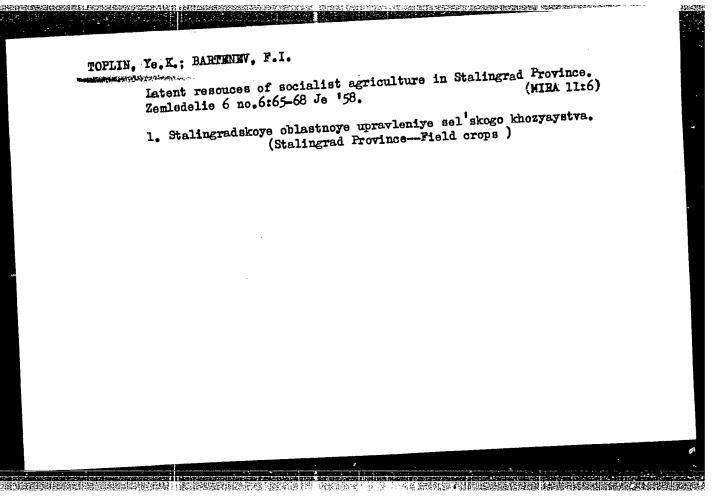
UDC: 576.858.25.093.3

CIA-RDP86-00513R001756310014-3" APPROVED FOR RELEASE: 08/31/2001

GORSHKOV, M.I.; ZINOV'TEV, V.R.; TOPLIN, A.I.; USHERKNKO, Z.I.

Cutting surfaced veneer with planer saws. Der.prom. 5 no.8:3-4
(MIRA 9:10)

Ag '56.
(Veneers and veneering) (Ploning machines)



TOPLIVA, A. M.

PA 4T45

Apr 1947

USSR/Fuels - Analysis

Coal

Furnaces

"Results of an Investigation of Stratified Combustion of Lignites on an Inclined Grate," D. G. Fayershteyn, A. M. Topliva, 6 pp

"Za Ekonomiyu Topliva" Vol IV, No 4

Gives full description with cross sections of boiler and furnace with which the grate is used. Graph of the coefficient of effective operation of the furnace and tables of the operating characteristics of the furnace with Kirovgrad and Alexandriysk coal.

TOPOL', A., (Engr-Col)

Listed as author of article, "Maintenance of Vehicles in Training Classes," which appears in <u>Tankist</u>, No 5, May 1954. (Sovetskaya Armiya, Group of Soviet Forces, Germany, 25 May 54).

SO: SUM No. 208, 9 Sep 1954

Z/034/62/000/001/004/011 E112/E435

AUTHOR:

Topol, Jan

TITLE 3

Prospects for the production of magnesium from domestic ores by the ferrosilicon thermal reduction

method

PERIODICAL: Hutnicke listy, no.1, 1962, 49-52

Abundant and easily accessible supplies of dolomite limestone are available in Czechoslovakia. investigations have established their suitability for the production of magnesium by the silicon reduction method and the present paper describes a semi-technical production unit. following individual steps are studied in detail: 1) crushing of the dolomite; 2) roasting; 3) milling and sieving; 4) mixing; 5) production of briquets from roasted dolomite, ferrosilicon and fluorspar; 6) heating under high vacuum and 7) distillation and refining of magnesium. Ad 1) and 3); it was seen that existing conventional machinery could be used successfully. Ad 2): course of roasting of the dolomite was studied and storage problems of the calcined materials were investigated. Ad 5); this operation is very critical with reference to yields and smooth Card 1/3

Z/034/62/000/001/004/011 E112/E435

Prospects for the production ...

No completely satisfactory method for the production of the briquets is known. Excessive pressures during briquetting reduce the escape of magnesium vapours, lowering the yield and increasing costs. Briquets, on the other hand, are harder and less prone to break during transport. (Low-strength briquets may lower the efficiency of the reduction furnace by as Briquetting in two stages is suggested. pressure for a charge consisting of calcined dolomite, 75% ferrosilicon and fluorspar was 1000 to 1100 kg/cm2. Ad 6): Reduction furnaces comprised four retorts made of austenitic steel. dimensions: total length, including the 500 mm condenser 2500 mm; inner diameter = 250 mm; wall thickness = 29 mm. Optimum charge of briquets: 65 kg. The minimum life of the retort is given as 1 year. Thermal reduction was carried out at 190°C and a vacuum of 5 x 10°2 torr. The effect of varying the Ca/MgO ratio on the course of the reduction and on the Carcontents in the condensed Mg were investigated: it was found that increasing amounts of CaO, up to a molar ratio 1.5 CaO: 1 MgO; had no effect on the Ca contents of the condensed Mg. Higher quantities of CaO produced a steep increase of Ca in the Card 2/3

Prospects for the production

Z/034/62/000/001/004/011 E112/E435

condensate. Raw-material and energy consumption of the pilot plant production unit are tabulated and compared with world average data. Results are practically identical except that the heat consumption was higher (5000 kcal/1 kg Mg, as against 4500 kcal). Considerably more favourable results were then obtained by constructing another furnace, heated electrically with graphite rods. Charge: 100 kg of briquets. The following comparative figures for the production of 1 kg Mg are given (kilowatt-hours); world average 20, Czechslovak pilot plant 12; (reduction time in hours); world average 48, Czechoslovak 7. The purity of the refined metal was 99.9% Existing raw materials and equipment combined with the experience gained in the pilot plant experiments are a sound basis for the industrial production of magnesium in Czechoslovakia There are 8 figures, 3 tables and 5 references: 4 Soviet-bloc and 1 non-Soviet-bloc. The reference to an English language publication reads as follows: Ref. 3: L.M. Pidgeon. J.A. King. Discussions Faraday, Soc., no.4, 1948, 197-206.

ASSOCIATION: VUK - Panenske Brežany

SUBMITTED: May 20, 1961

Card 3/3